

# Simplified Sizing Procedure For Solar Domestic Hot Water Systems



Florida Solar Energy Center

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The following procedure was developed to size residential solar water heating systems in Florida.  
See last page for limitations and assumptions.

## Hot water demand and tank size

**Step 1.** Using Table 1, estimate daily hot water use (GALLONS) and select a nominal tank size (TANK SIZE).

\_\_\_\_\_ gal/day  
GALLONS (1)

\_\_\_\_\_ gal  
TANK SIZE

**Table 1. Hot water demand and tank size**

Average GALLONS and minimum TANK based upon number of people **or** bedrooms:

People (or)	Bedrooms	GALLONS	Minimum TANK SIZE (Gallons)
1		20	40
	1	30	30
2		40	40
	2	50	52
3		55	52
	3	70	80
4		85	80
	4	90	100
5		100	100
	5	110	120
6		115	120

(Add 15 gallons for each additional person.)  
(Add 20 gallons for each additional bedroom.)

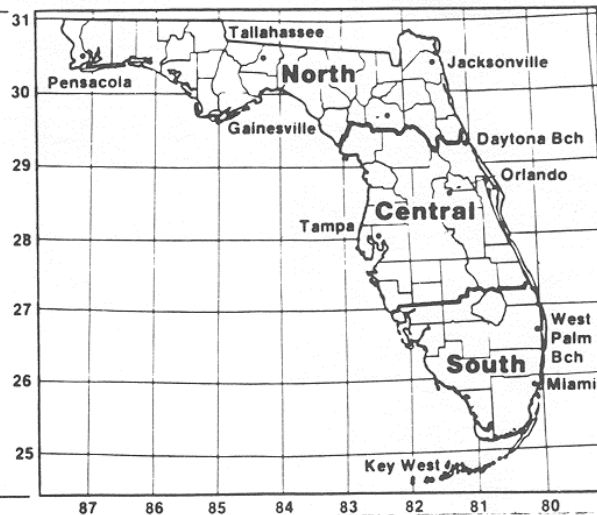
**Step 2.** Using Figure 1, determine the proper cold water temperature (COLDTEMP) for location.

\_\_\_\_\_ °F  
COLDTEMP (2)

**Figure 1. Cold water temperatures**

Region	COLDTEMP
North Florida (1, 2, 3)*	68°F
Central Florida (4, 5, 6)*	72°F
South Florida (7, 8, 9)*	76°F

\* Correspond to regions for the Florida model energy building code.



**Step 3.** Calculate how much energy is needed (BTUNEED) to heat the water to 122°F.

$$BTUNEED = 8.34 \times \text{GALLONS} \times (122 - \text{COLDTEMP}) \times \text{Standby loss factor}$$

$$BTUNEED = 8.34 \times \frac{\text{GALLONS}}{(\text{Step 1})} \times (122 - \frac{\text{COLDTEMP}}{(\text{Step 2})}) \times \frac{\text{Standby loss factor}}{(\text{Table 2})} = \frac{BTUNEED}{(\text{3})} \text{ Btu/day}$$

**Table 2. Standby heat loss from storage**

Type of tank insulation	Standby loss factor
1-in. foam or 2.5-in. fiberglass (R = 8 - 9)	1.20
2-in. foam (R = 16 - 17)	1.12

(Use linear interpolation to obtain standby loss factor for insulation materials having other R-values.)

Table 2 is to be used for sizing systems with FSEC rating. If SRCC rating is used and if there are no other backup tanks then use a standby loss factor of 1.0.

**Example:** A thermosiphon water heater with its storage tank containing a back-up element has an SRCC rating. There are no other back-up tanks for the system. In this case use a standby loss factor = 1.0

**Example:** The same thermosiphon water heater system is used as a preheater to another back-up tank. The element in the thermosiphon tank may not be connected. In this case use a standby loss factor from Table 2 corresponding to back-up tank insulation levels.

### Collector Sizing

**Step 4.** Determine penalty factors that affect sizing.

- a. Select the System Factor from Table 3.

$\frac{\text{System Factor}}{\text{System Factor}} \quad (4a)$

- b. Select the proper Tilt Factor from Table 4.

$\frac{\text{Tilt Factor}}{\text{Tilt Factor}} \quad (4b)$

- c. Select the Orientation Factor from Table 5.

$\frac{\text{Orientation Factor}}{\text{Orientation Factor}} \quad (4c)$

Calculate the overall penalty factor (PENALTY) for the combination of all three individual effects:

$$PENALTY = \text{System Factor} \times \text{Tilt Factor} \times \text{Orientation Factor}$$

$$PENALTY = \frac{\text{System Factor}}{(\text{Step 4a})} \times \frac{\text{Tilt Factor}}{(\text{Step 4b})} \times \frac{\text{Orientation Factor}}{(\text{Step 4c})} = \frac{PENALTY}{(\text{4})}$$

**Table 3. System factors**

System configuration	System factor
Direct system with no heat exchanger.	1.20
Indirect system with a heat exchanger between collector and storage tank.	1.30
Systems with SRCC system certification and Q <sub>NET</sub> rating.	1.00

**Table 4. Tilt factors**

Collector tilt			Tilt factors		
Tilt angle	Roof pitch	Roof tilt	North Florida	Central Florida	South Florida
0° to 3°	0	0°	1.25	1.22	1.19
3° to 7°	1 in 12	4.8°	1.15	1.14	1.12
7° to 12°	2 in 12	9.5°	1.09	1.08	1.06
12° to 16°	3 in 12	14.0°	1.05	1.04	1.03
16° to 20°	4 in 12	18.4°	1.02	1.01	1.01
20° to 25°	5 in 12	22.6°	1.00	1.00	1.00
25° to 30°	6 in 12	26.6°	1.00	1.00	1.00
30° to 37°	8 in 12	33.7°	1.01	1.01	1.02
37° to 43°	10 in 12	39.8°	1.04	1.05	1.06
43° to 50°	12 in 12	45.0°	1.08	1.10	1.12

**Table 5. Orientation factors**

Collector orientation	Orientation factor
South or nearly south	1.00
Southeast or southwest	1.15
East or west	1.40

**Step 5.** Calculate the rating requirements of the solar system (RATREQD) to provide 70% of the annual hot water energy needs using the formula:  
 RATREQD = BTUNEEDED x 0.70 x PENALTY

$$\text{RATREQD} = \frac{\text{BTUNEEDED}}{\text{(Step 3)}} \times 0.70 \times \frac{\text{PENALTY}}{\text{(Step 4)}} \quad \text{RATREQD} \quad \text{Btu/day (5)}$$

**Step 6.** For the collector selected, record the thermal performance rating at the intermediate temperature (BTURATING) in Btu/day and the gross collector area (GROSSAREA) in square feet from the required FSEC label.

Collector Manufacturer \_\_\_\_\_

Model No. \_\_\_\_\_

Thermal Performance Rating at the Intermediate Temperature (Btu/day) or SRCC Q<sub>NET</sub> or Q<sub>NET</sub> equivalent\* \_\_\_\_\_ BTURATING Btu/day (6a)

Gross Collector Area (ft<sup>2</sup>) \_\_\_\_\_ GROSSAREA ft<sup>2</sup> (6b)

Estimate the number of collectors needed using:

$$\text{NUMBER} = \frac{\text{RATREQD}}{\text{BTURATING}} = \frac{\text{(Step 5)}}{\text{(Step 6a)}} \quad \text{NUMBER} \quad \text{(6c)}$$

**Step 7.** Select the actual number of collectors to be used. This is the nearest whole number to (6c).

\_\_\_\_\_ NO. COLLECTORS (7a)

The total area of the collector array is:

TOTAL AREA = NO. COLLECTORS x GROSSAREA

$$\text{TOTAL AREA} = \frac{\text{(Step 7a)}}{\text{(Step 7a)}} \times \frac{\text{(Step 6b)}}{\text{(Step 6b)}} \quad \text{TOTAL AREA} \quad \text{ft}^2 \quad \text{(7b)}$$

\*For those systems that are SRCC certified use the SRCC Q<sub>NET</sub> rating here. Systems with only an FSEC test and certification may get an equivalent SRCC Q<sub>NET</sub> from FSEC Testing & Operations on request.

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Based upon the actual number of collectors to be used, compute the solar fraction (SOLAR FRACTION):

$$\text{SOLAR FRACTION} = \frac{0.70 \times \text{NO. COLLECTORS}}{\text{NUMBER}} = \frac{0.70 \times \frac{\text{NO. COLLECTORS}}{\text{NUMBER}}}{\frac{\text{NO. COLLECTORS}}{\text{NUMBER}}} = \frac{\text{SOLAR FRACTION (7a)}}{\text{SOLAR FRACTION (6c)}} = \text{SOLAR FRACTION (7C)}$$

If the solar fraction (Step 7c) is less than 0.65, the collector array is undersized. Consider either adding another collector or using a different model/size collector.

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This procedure has several constraints:

1. The procedure is valid only for Florida
2. The procedure is based on sizing solar systems to provide between 65% and 75% of the heating load; i.e., a solar fraction of between 0.65 and 0.75. A solar fraction of 0.7 is estimated to be optimum for most installations and, in particular, for solar collectors with a tilt angle of approximately 20° to 25° (mounted parallel to the 4-in-12 or 5-in-12 pitched roofs that are common in Florida). The 20° - 25° collector tilt angle provides for an aesthetic installation and meets 100% of the hot water needed in summer and 50% in winter. Systems can be sized to maximize lifetime savings by providing a larger solar collector that will produce a solar fraction of 0.9 or higher. To achieve this solar fraction, the collectors will need to be installed at a tilt angle of between 40° and 50°.
3. The hot water delivery temperature of 122°F in step 3 was obtained by FSEC from analysis of two years of actual experimental data. The 122°F delivery temperature is consistent with Florida law, which requires that hot water thermostats be set no higher than 125°F. It is also consistent with electric water heater energy consumption data as measured by Florida Power and Light Co.

Automatic dishwashers may not clean dishes very well at 122°F. However, most dishwashers have a cycle that uses an electric element in the dishwasher to boost the water temperature to about 140°F.

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